

Ultra-light Vapor Fueled Cavity Reactors with MHD for Powering Multi-Megawatt NEP Systems

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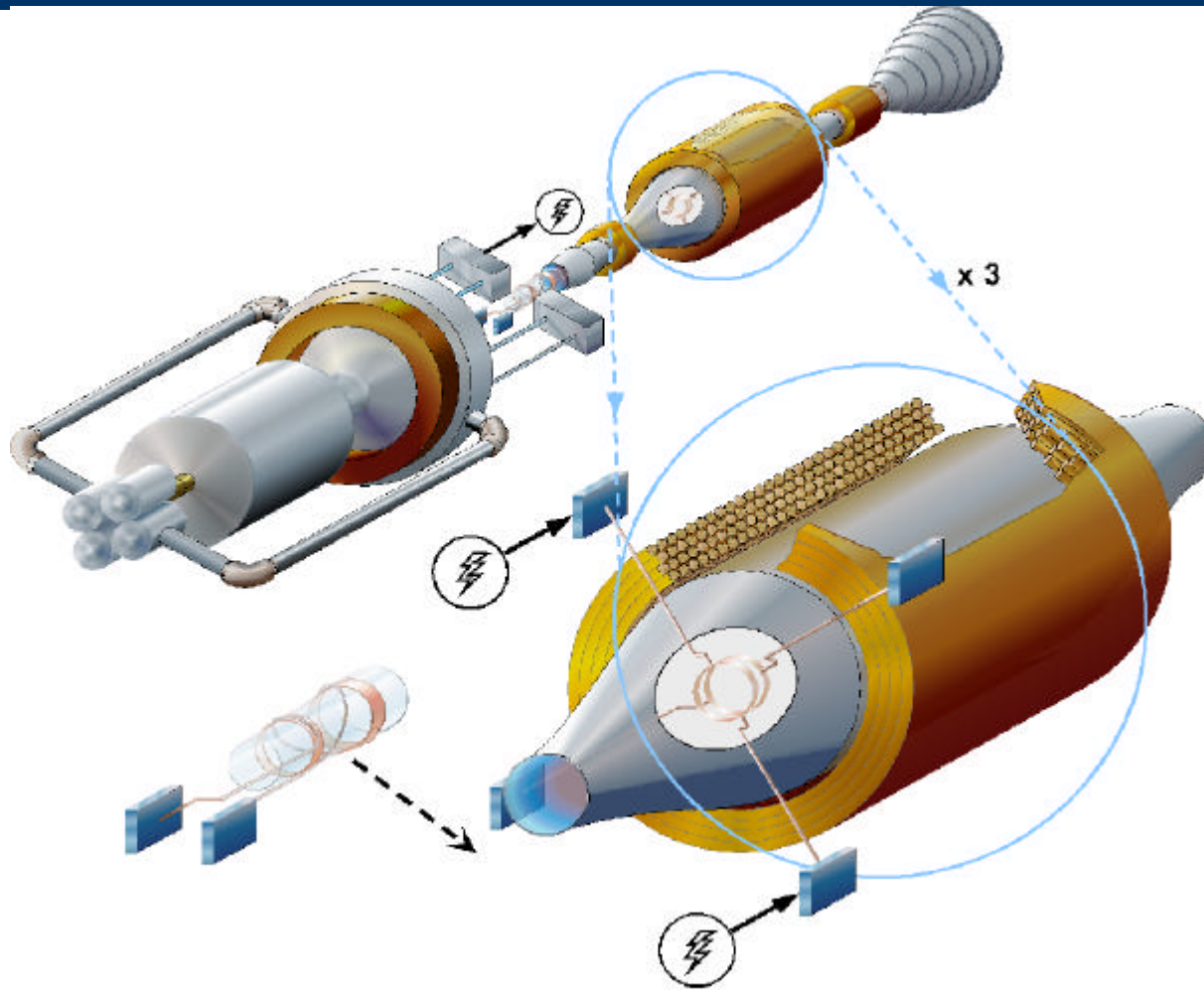
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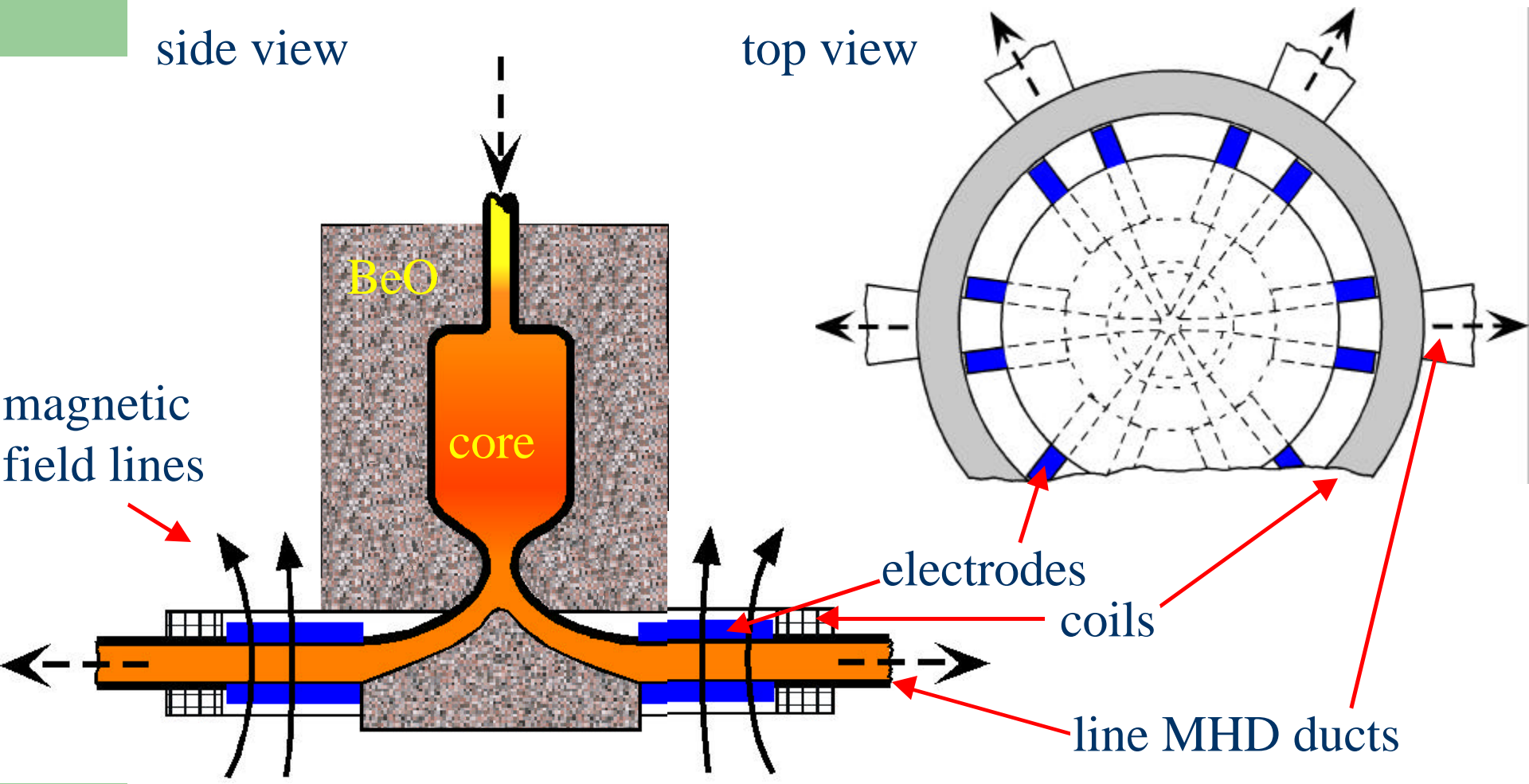


Innovative Nuclear Space
Power and Propulsion Institute

Overview of Nuclear MHD Power Conversion for Multi-MW Propulsion



Fissioning Plasma Core Reactor



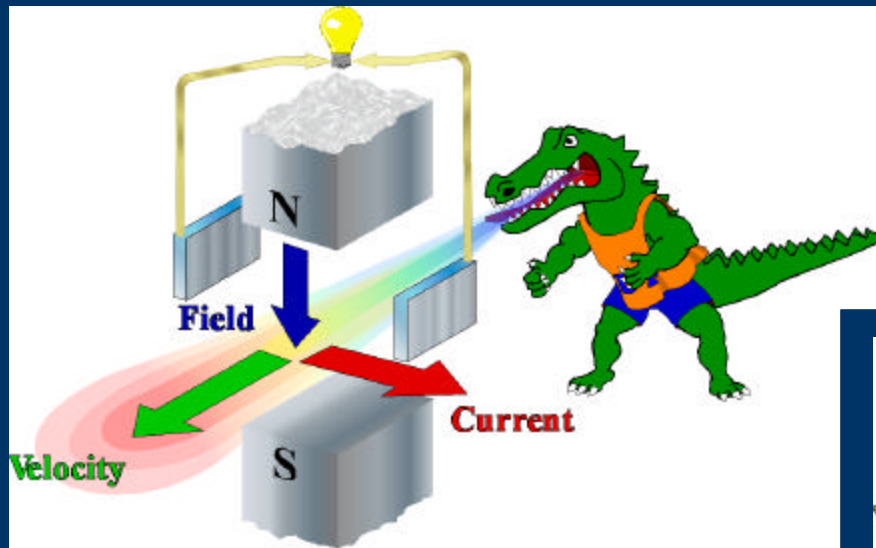
Overview - Fissioning Plasma Core Reactor with MHD (FPCR-MHD)

- Fissioning fuel, UF_4
- Working fluid, alkali metals or their fluorides (K, Li, Na, KF, LiF, NaF, etc.)
- Core Outlet T., 3000 to 4000 K
- Specific mass, 0.4 to 0.6 kg/kWe
- Power, 10 to 200+ MWe
- Coupling to MPD, VASIMR, other thruster
- Isp, 1500 to 10,000 s.

Advantages of Gaseous/Liquid Fuel

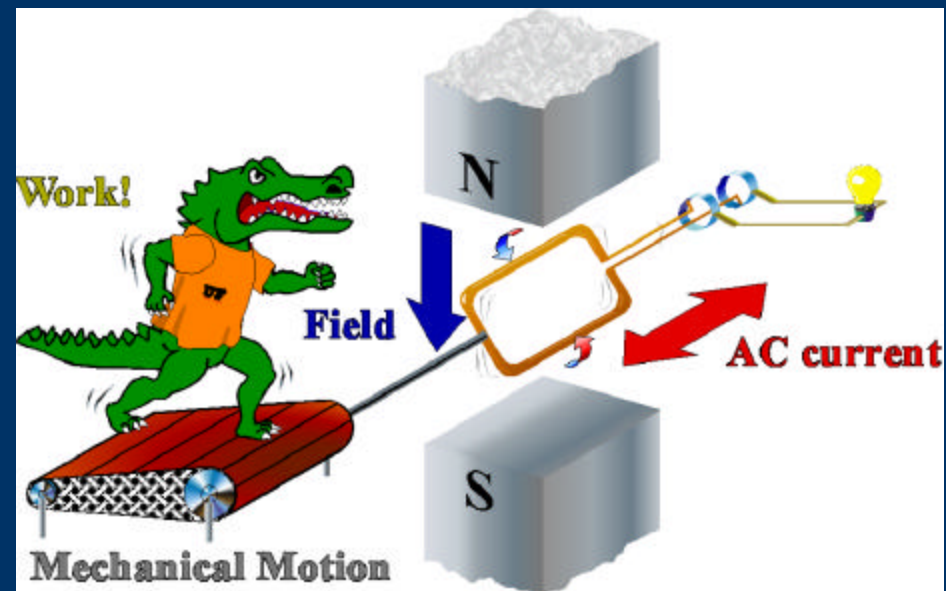
- In space assembly, fueling and refueling
- Ultra-safe fuel handling and delivery
- Operating temperature not constrained by fuel melting
 - high efficiency
 - minimizes radiator size/weight
 - no heat transfer barriers between fuel & working fluid
- Power scaling by varying fuel recirculation rate and average fuel exit temperature
- High temperature cavity reactor with integrated containment and moderator/reflector structure as well as integrated fuel/heat transport leading to very low kg/kWe

The Principle of MHD Generators



- MHD generator
 - Only twice downgraded.

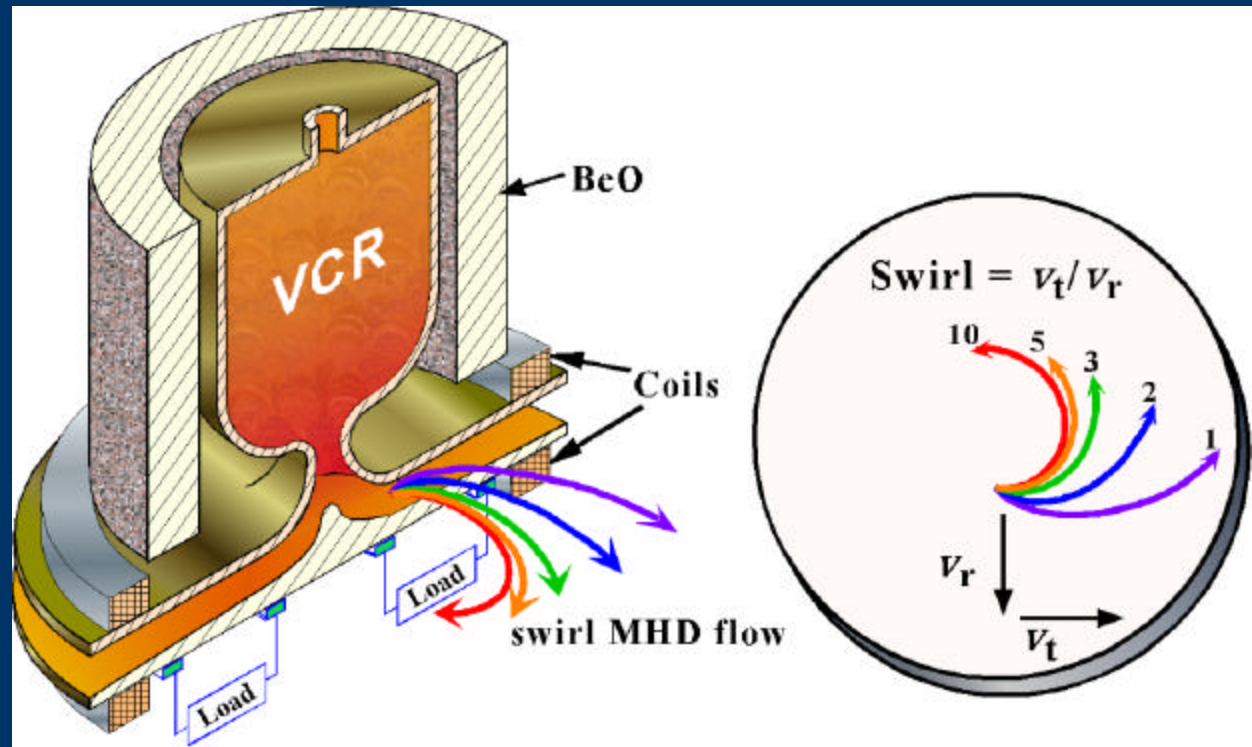
- Steam turbine
 - At least 3 downgrades.



Nuclear MHD Power Generation

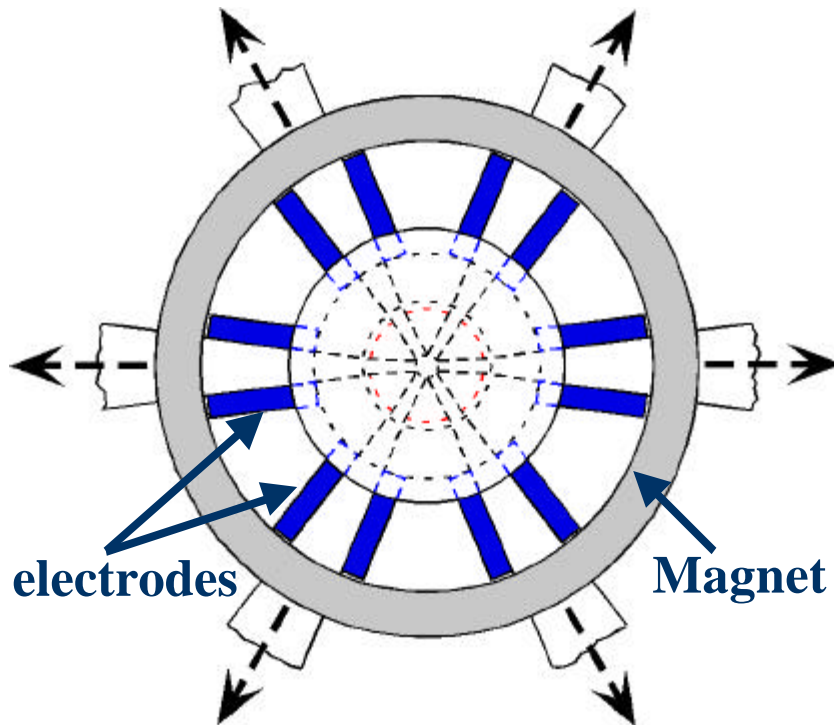
- No moving parts, high temperature cycle
- Utilize energy in its highest quality before degraded to heat
- Enhanced electrical conductivity of working fluid by fission-induced non-equilibrium ionization
- Minimum power conditioning needed – direct coupling with MPD, VASIMR or other thrusters

Disk VCR-MHD Generator

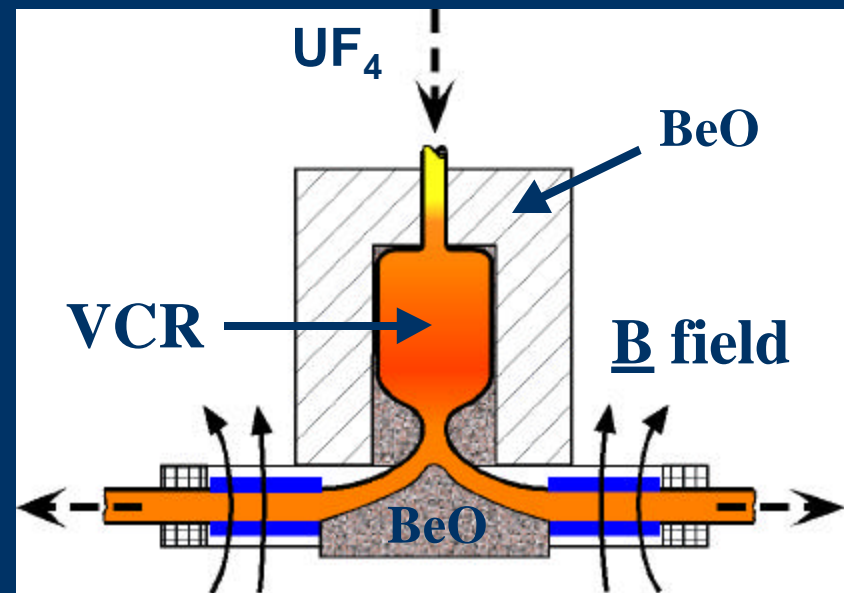


- Hall regime, efficiency increases with $\omega t = nB$.
- Hall efficiency increases with swirl (ie. tangential velocity).

Radial Line MHD Generator



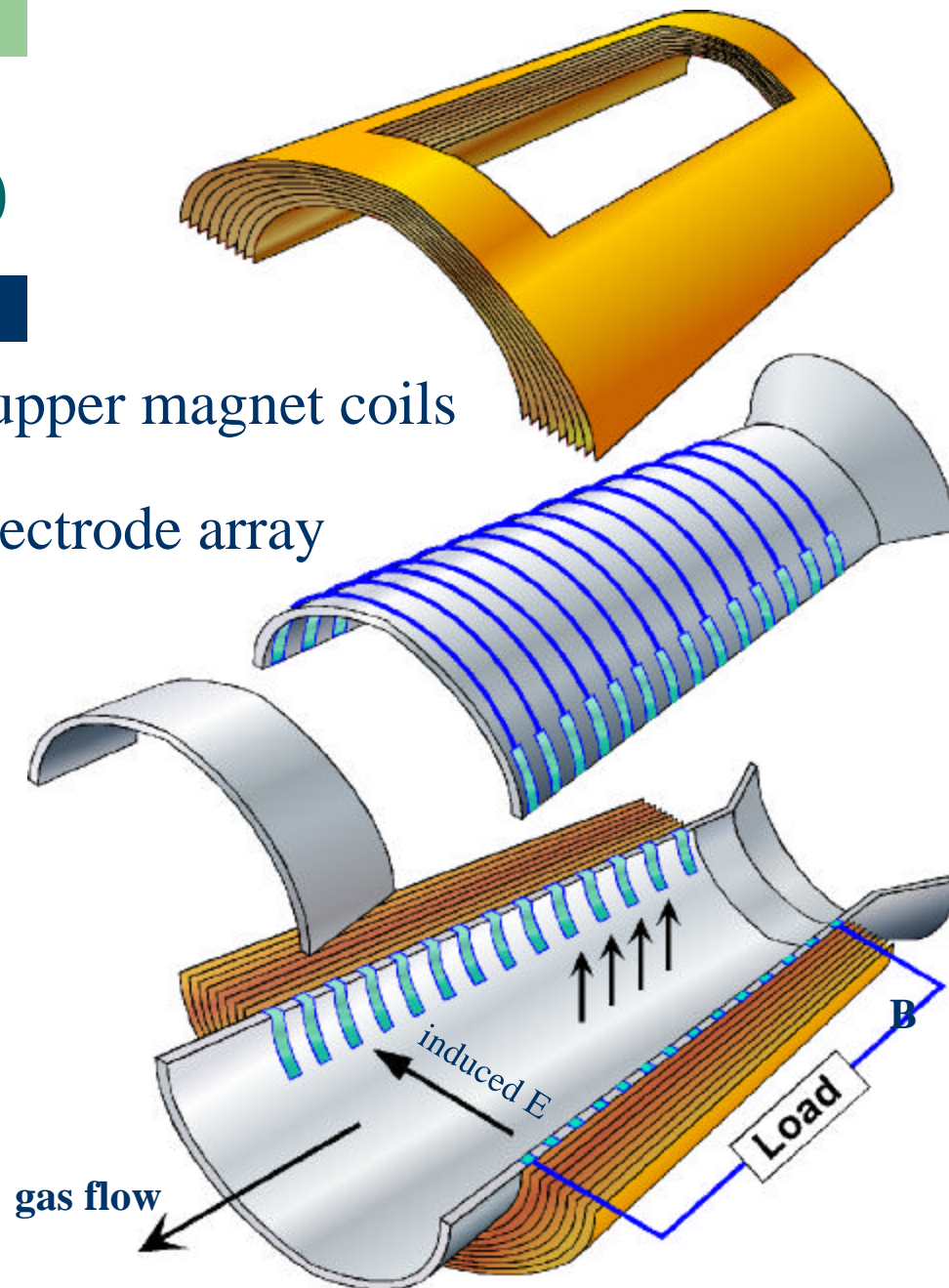
- Simpler design than disk swirl generator.
- No swirl flow required.



Line MHD

upper magnet coils

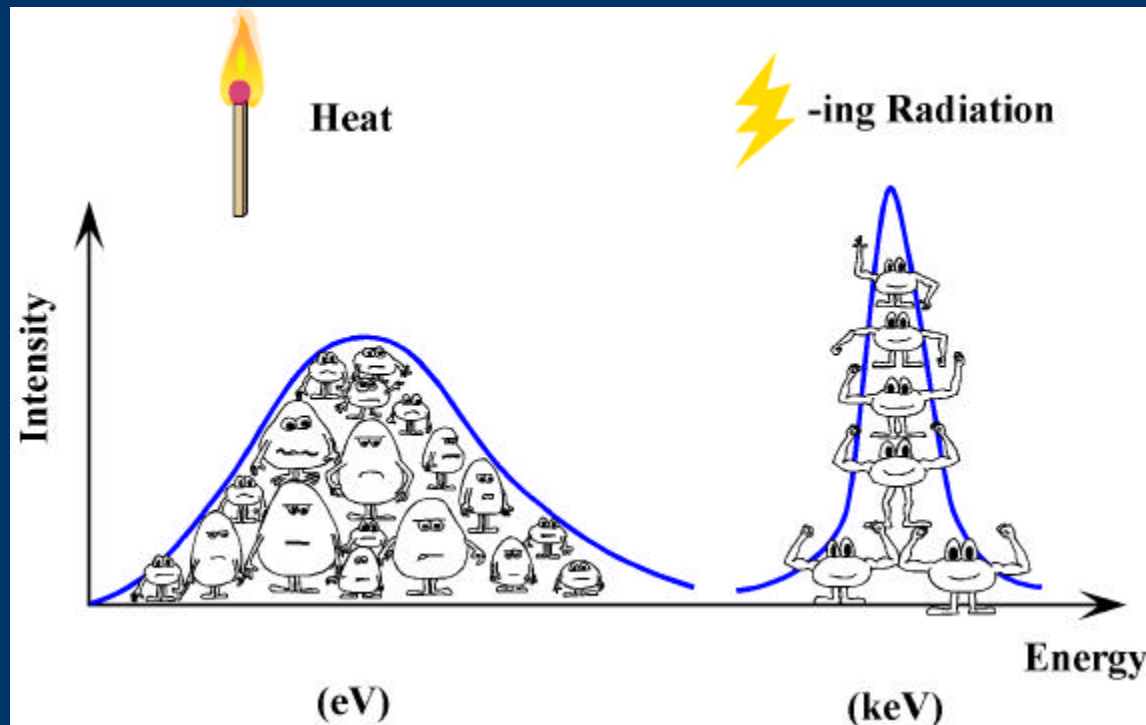
Hall-type electrode array



Plasma Electrical Conductivity

- $\sigma = ne$
- Losses $\propto n^2$.
- $\sigma =$ electric conductivity, $n =$ electron density, $\mu =$ *electron mobility*.
- *MHD Power Density* $= \sigma v^2 B^2$
- To minimize losses, n should be Low.
- In Nuclear MHD B^2 could be High.

Fission Product Ionization



Fission radiative:
Fewer but “power”
workers.

Thermal :
Large number of
“lazy” workers.

- Saha equation for thermal ionization, $n_e n_i \sim T^{3/2} \exp(-e/kT)$, gives \sim KeV or less.
- Fission product radiation, average β -energy \sim 900 keV.
 \therefore Fission enhanced conductivity, $\sigma \sim T^{3/2} \Phi^{1/3} T_e$

Some MHD Generator Characteristics

- MHD length
 $L = L(\mathbf{s}, \mathbf{B})$.
- - $\mathbf{B} \perp \mathbf{s}$ for
same L .

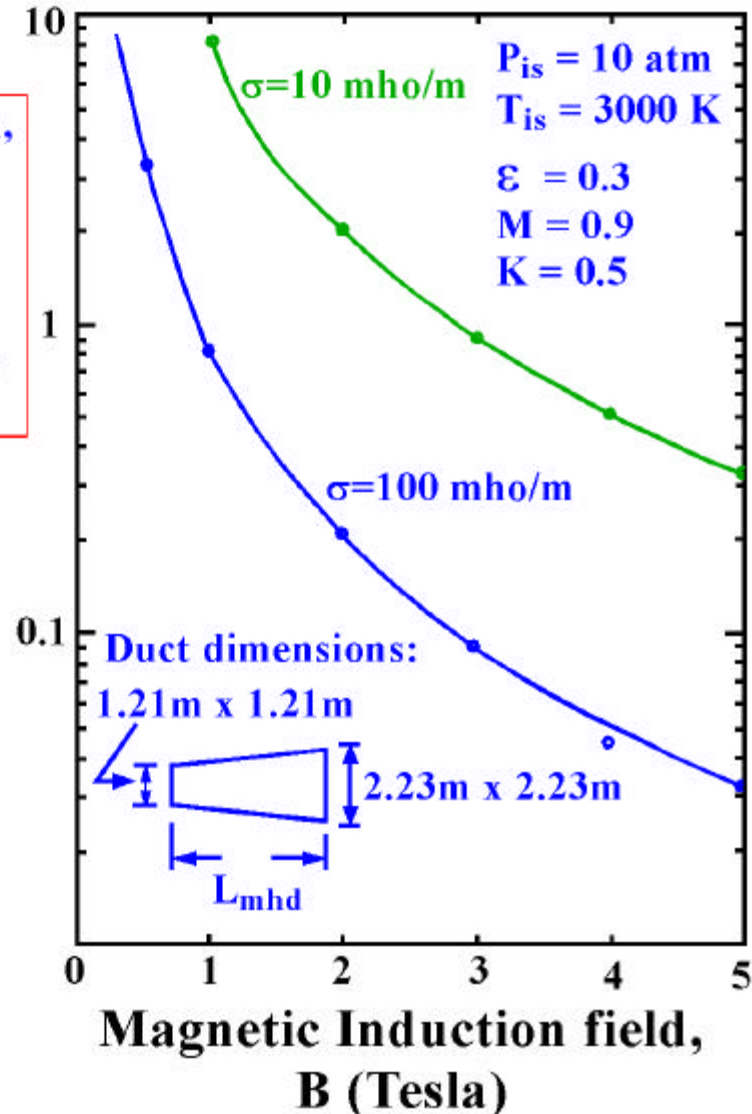
Symbols Legend:

Enthalpy extraction,
 $\epsilon = \Delta H_{\text{mhd}}/H_o$

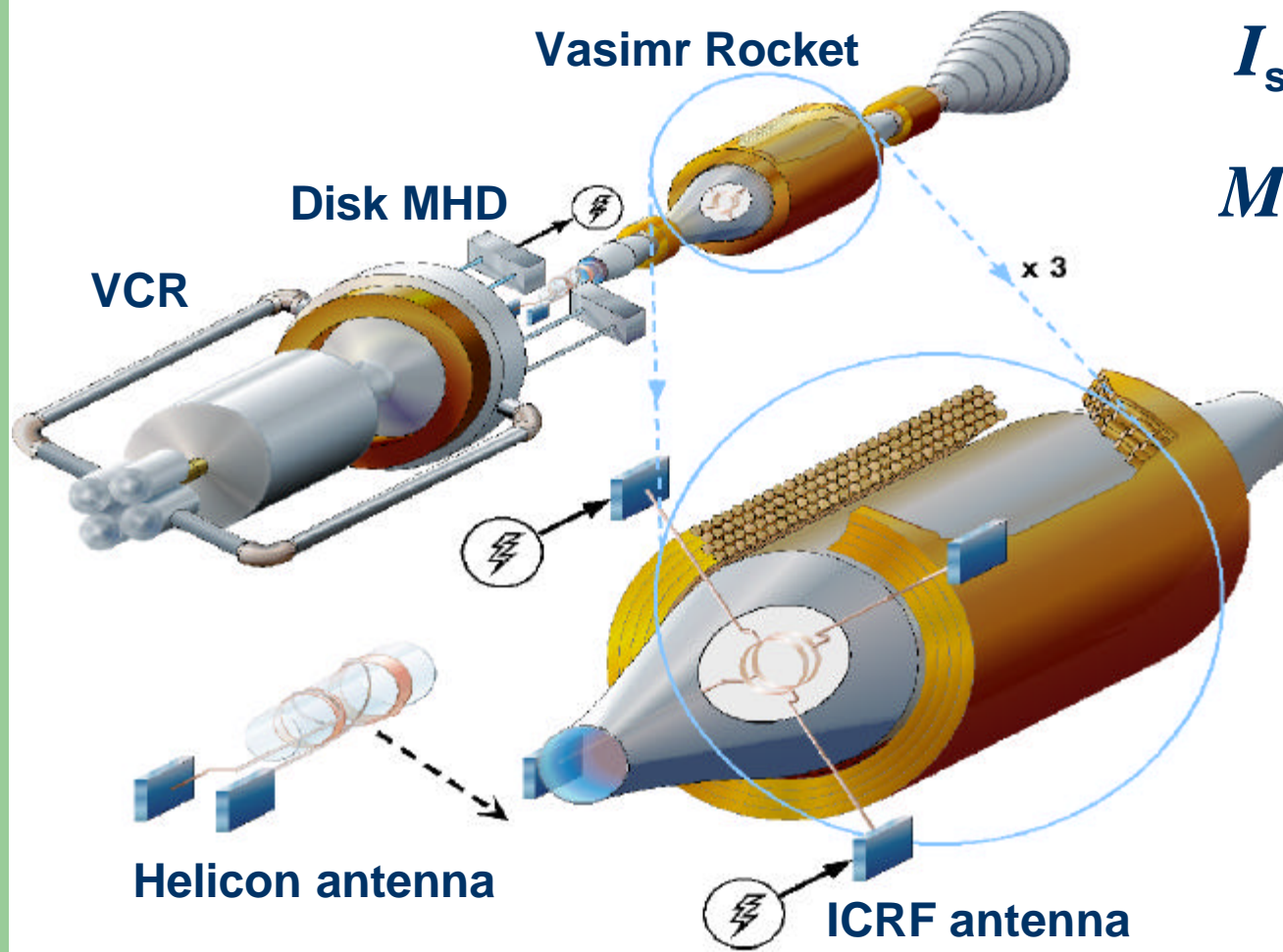
Sonic Mach
number = M

Loading parameter,
 $K = E_y/(uB)$

MHD Generator
Length (m)



Fully Integrated VCR-MHD-VASIMR NEP System

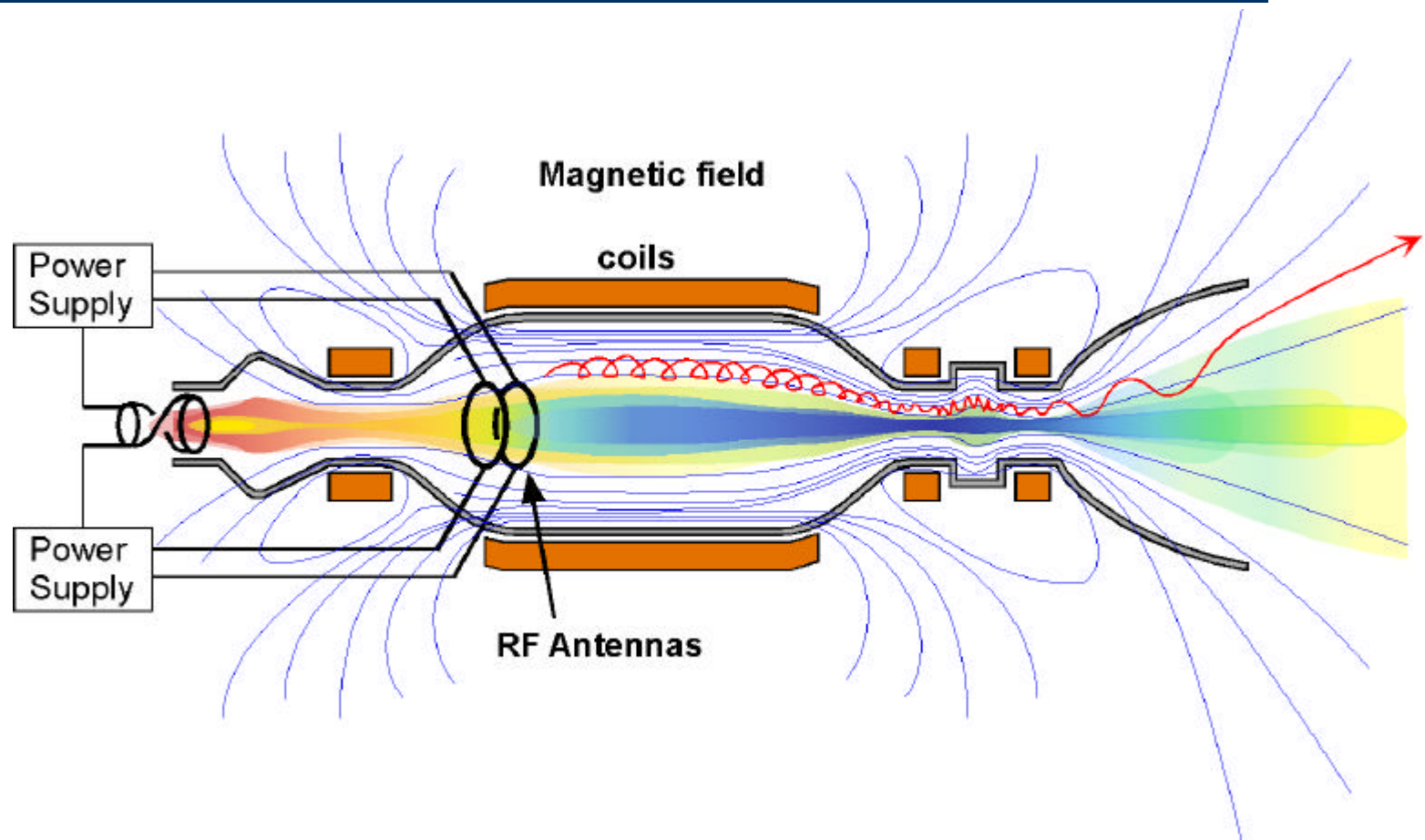


$$I_{sp} \sim 10,000 \text{ s}$$

$$M_{sp} \text{ £ } 1.0 \text{ kg/kW}_e$$

... Specific Concepts, part 2: *VASIMR*

Variable Specific Impulse Magnetoplasma Rocket



Propulsion using magnetic mirrors in VASIMR.

Nuclear MHD Power and NEP

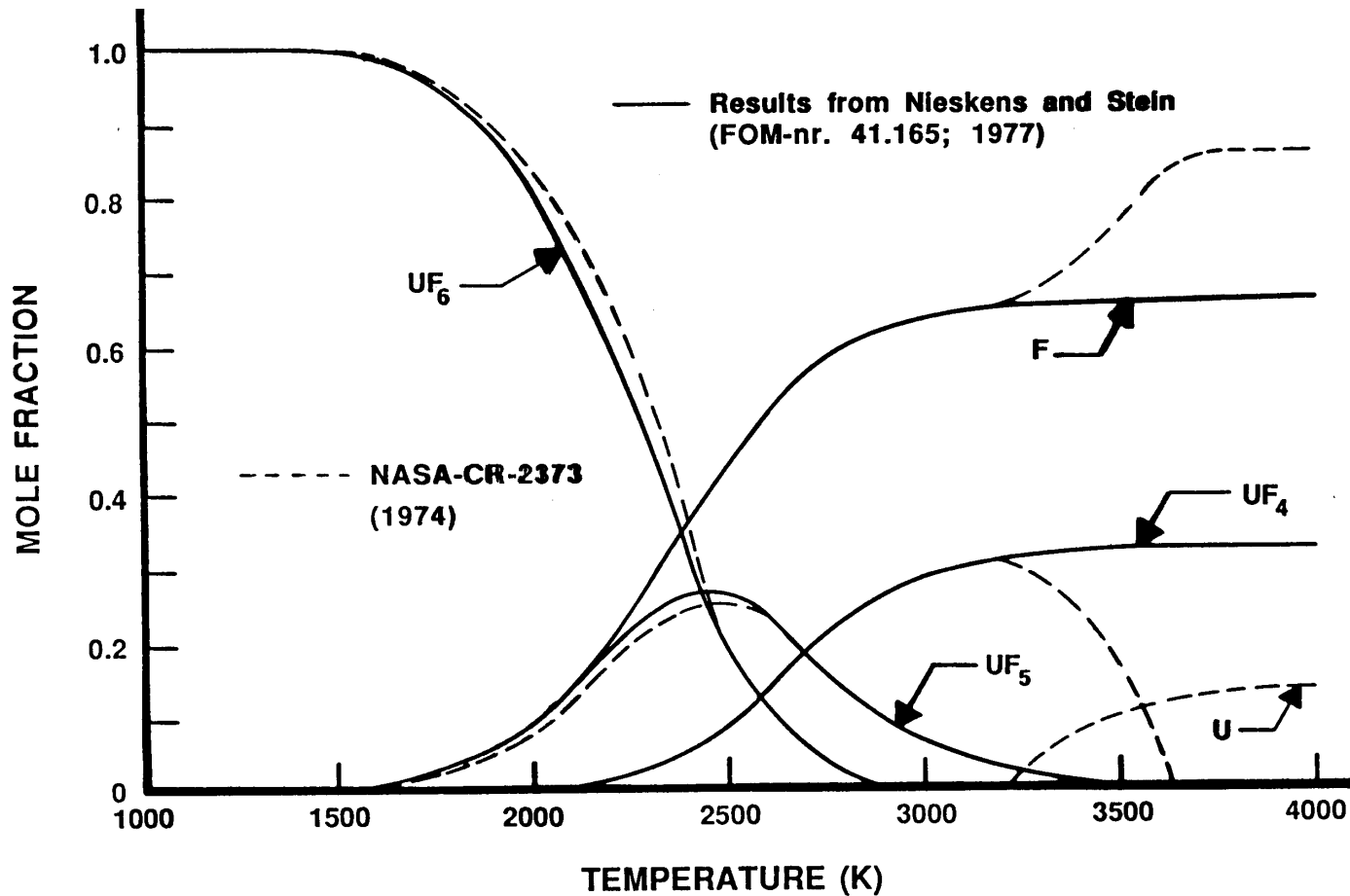


- High power density in gas core reactors.

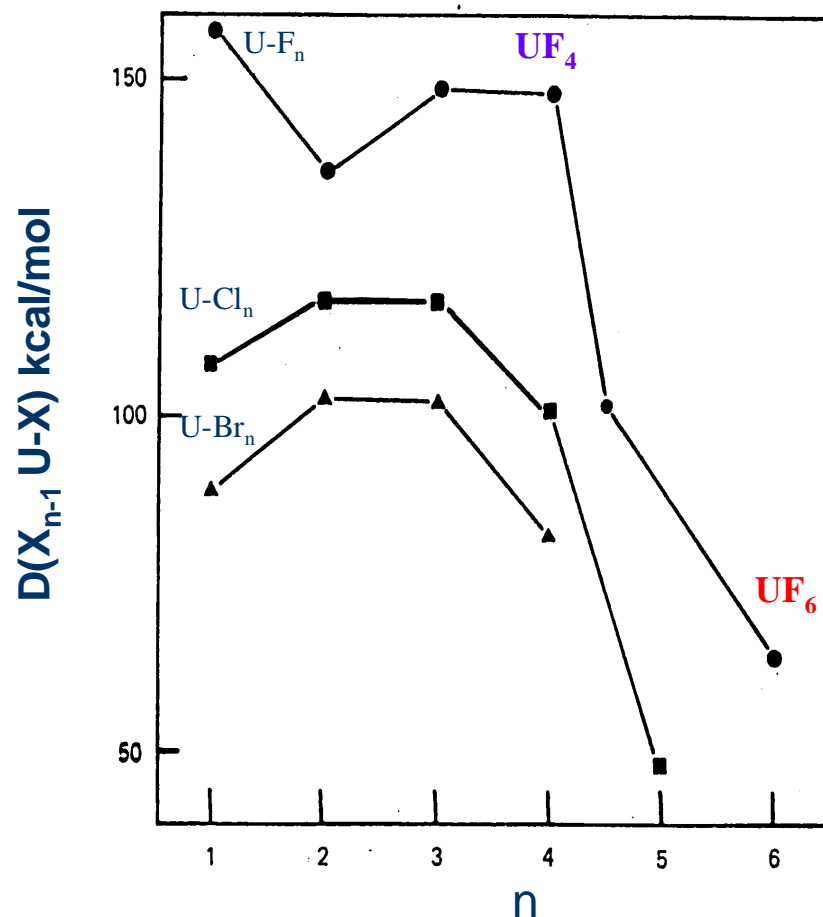


- Heat rejection at higher temperature,
 - Size of radiators can be reduced.
- Low specific mass,
High specific impulse,
 - Meets Mars quick trip requirements.

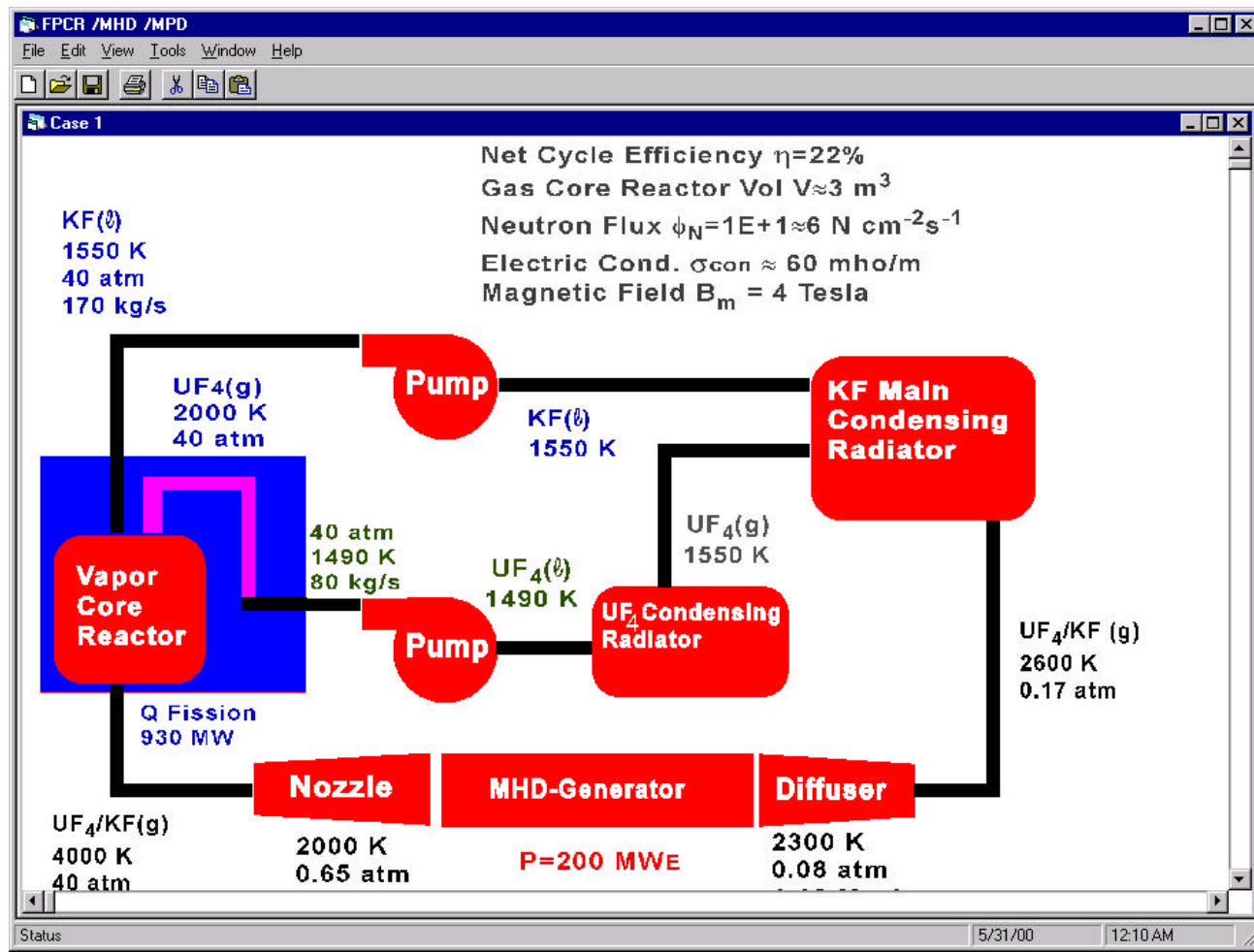
U-F system, UF_4 the most stable uranium compound in liquid and gaseous phase



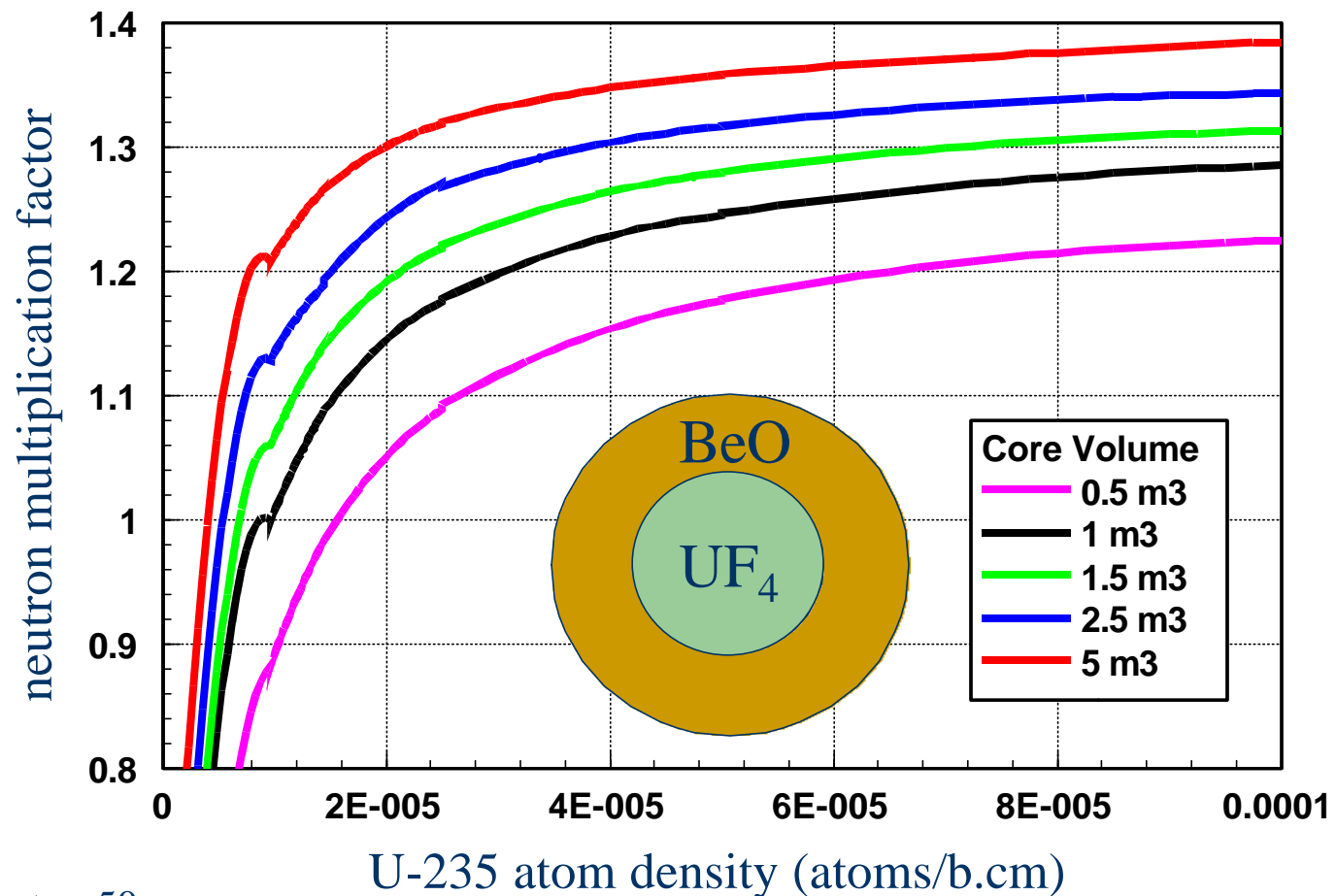
U-F_n Bond Dissociation Energies



Fissioning Plasma Core Reactor Simulation Code

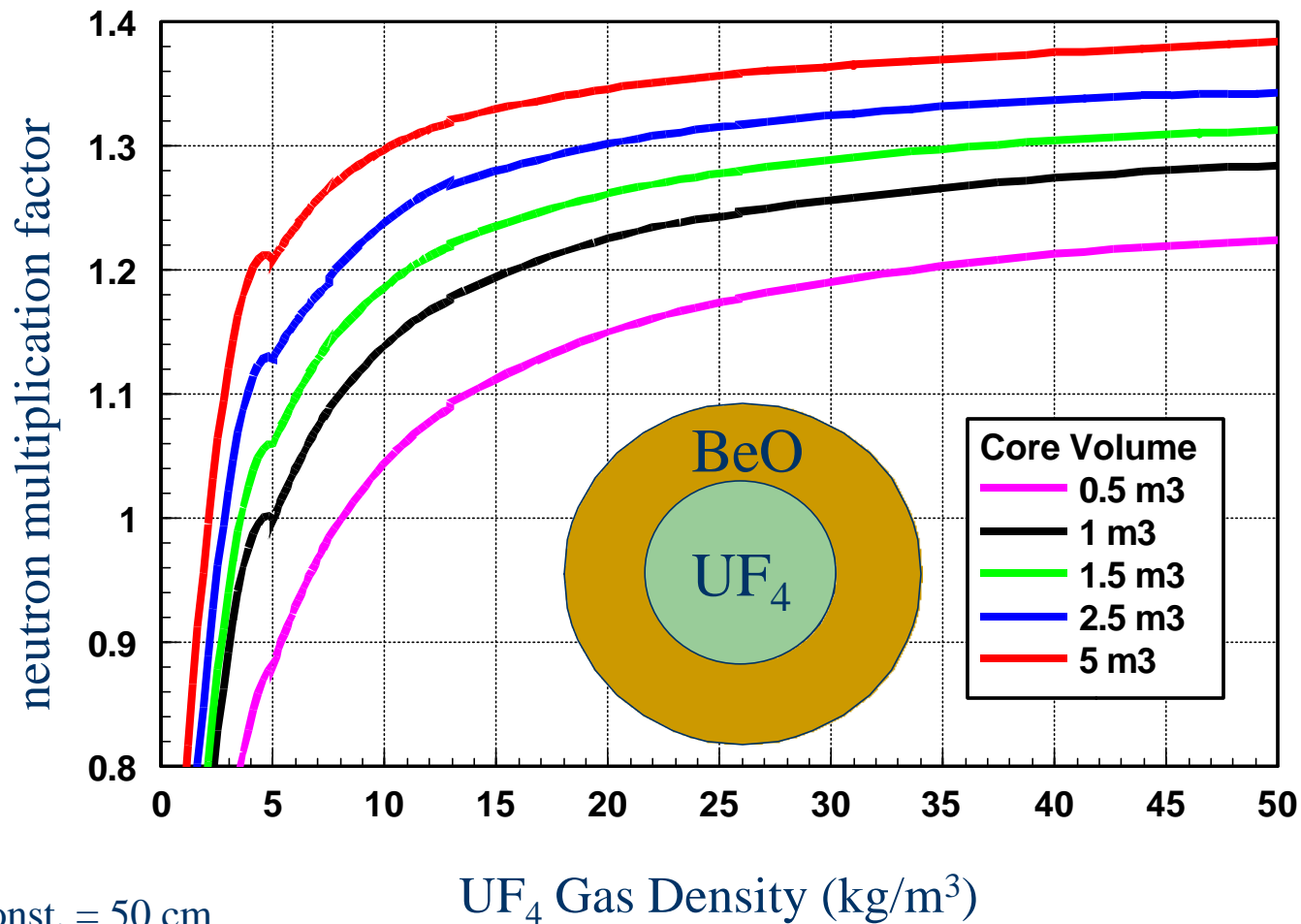


Cavity Reactor – Neutron Multiplication Factor



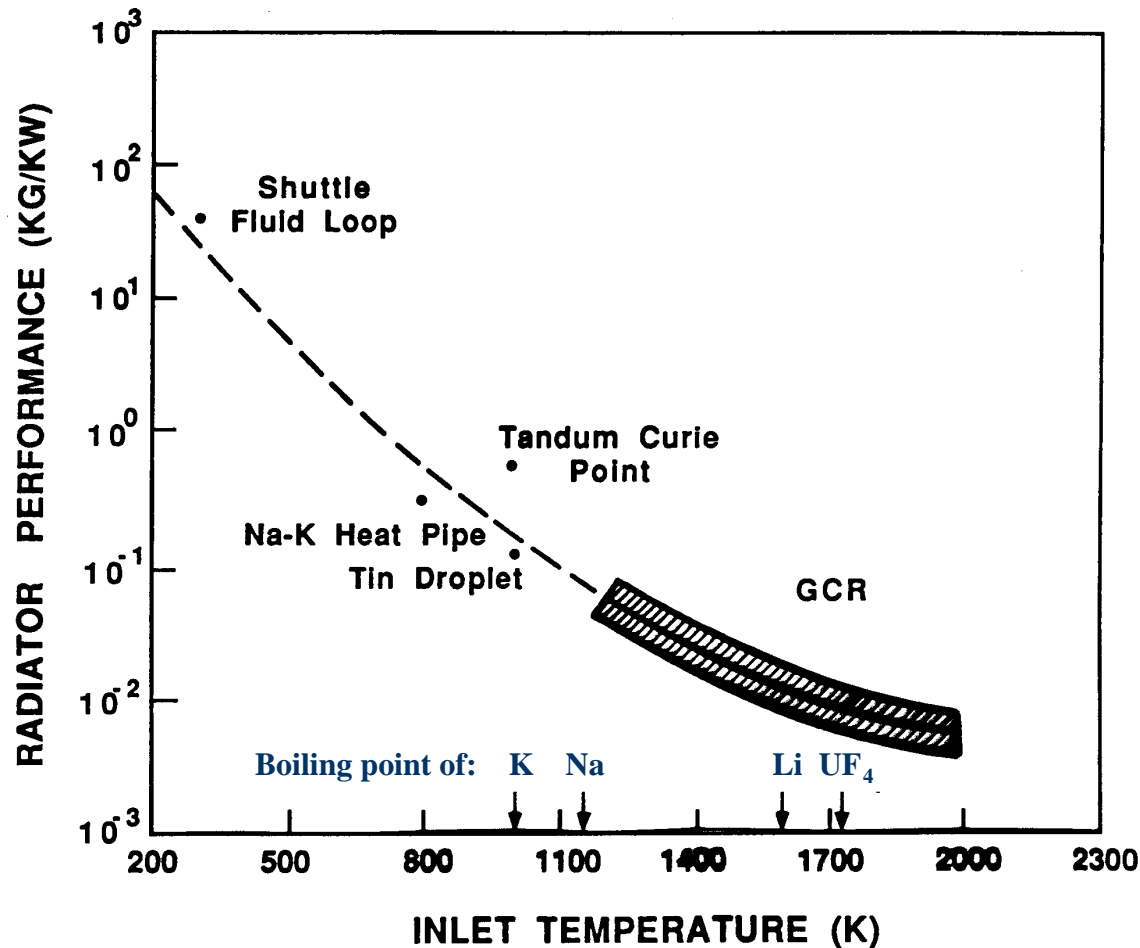
BeO thickness = const. = 50 cm

Cavity Reactor – Neutron Multiplication Factor



BeO thickness = const. = 50 cm


Radiator Mass to Power Ratio



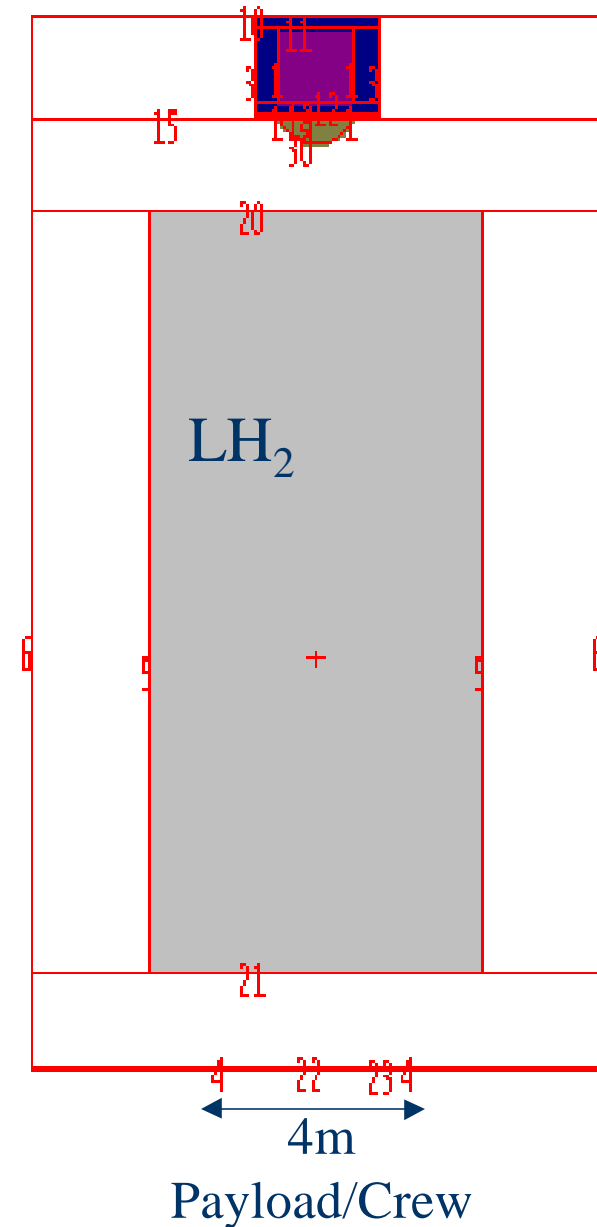
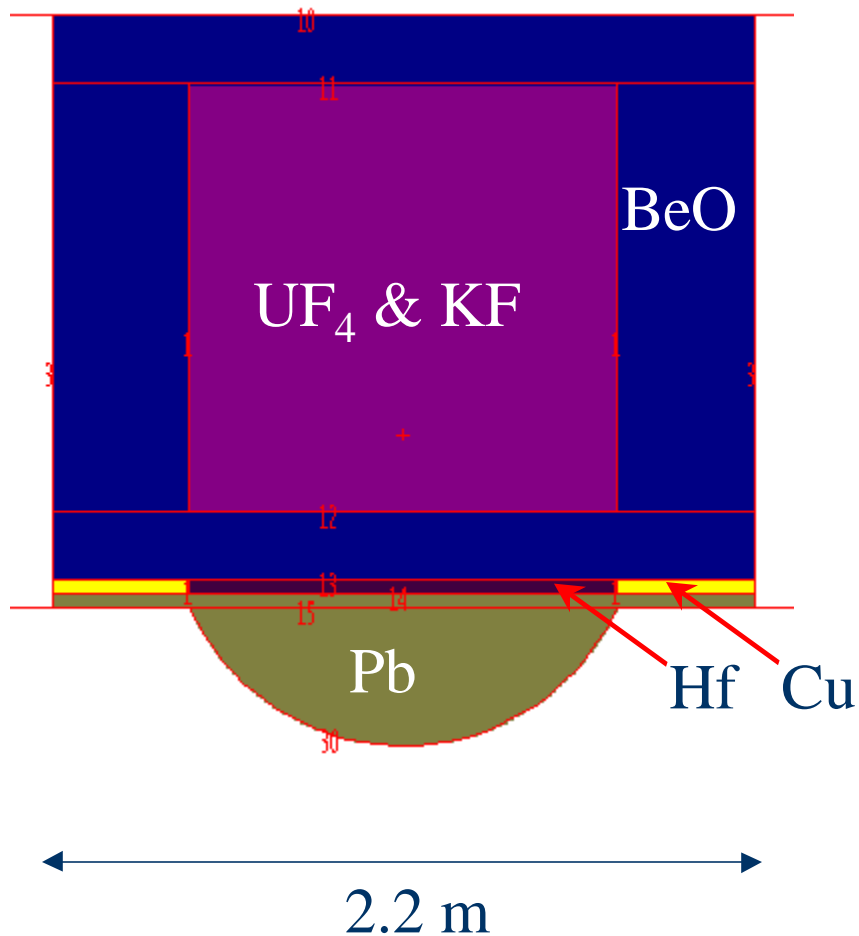
Specific Mass Calculation

- Core & Reflector
- Reactor Vessel & Structural Materials
 - Stainless steel
 - TZM (Mo99/Ti0.9/Zr0.1), Mo-Ti alloys
 - Ti-Al alloys
- Radiation Shield (Pb,Cu,Hf,polyethylene,B₄C)
- Radiators
- MHD Generator
- Pumps and plumbing

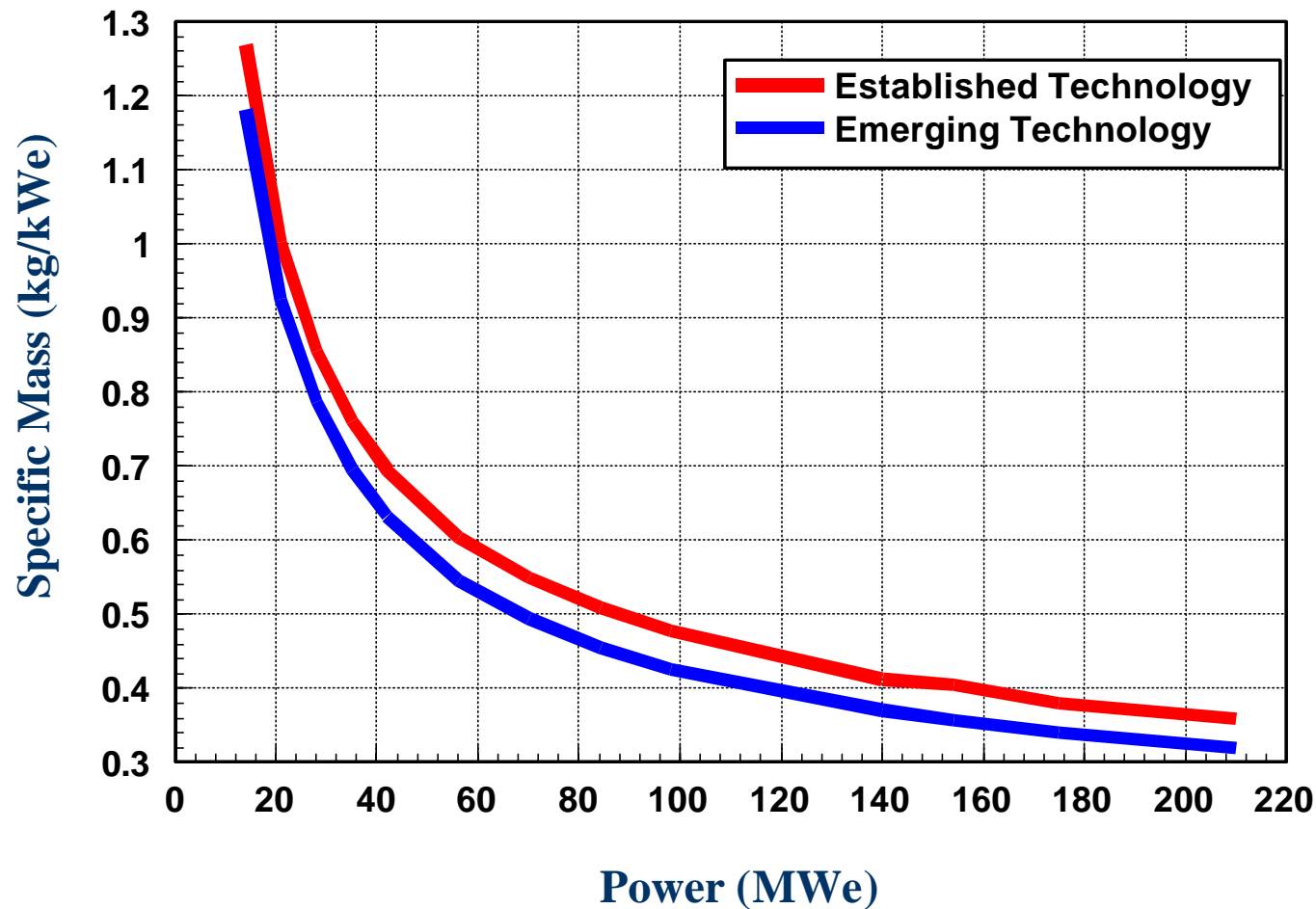
Radiation Shielding Calculation

- Laminated Pb/Hf/Cu planar and semi-circular shield with additional polyethylene shielding for crew
- Additional Shielding possible with L H₂ tanks between reactor and payload/crew module (typically 50 MT)
- Sources – neutrons and photons from fission
 - Neutrons – Watt fission spectrum (incl. prompt & delayed)
 - Photons – including prompt & decay -rays

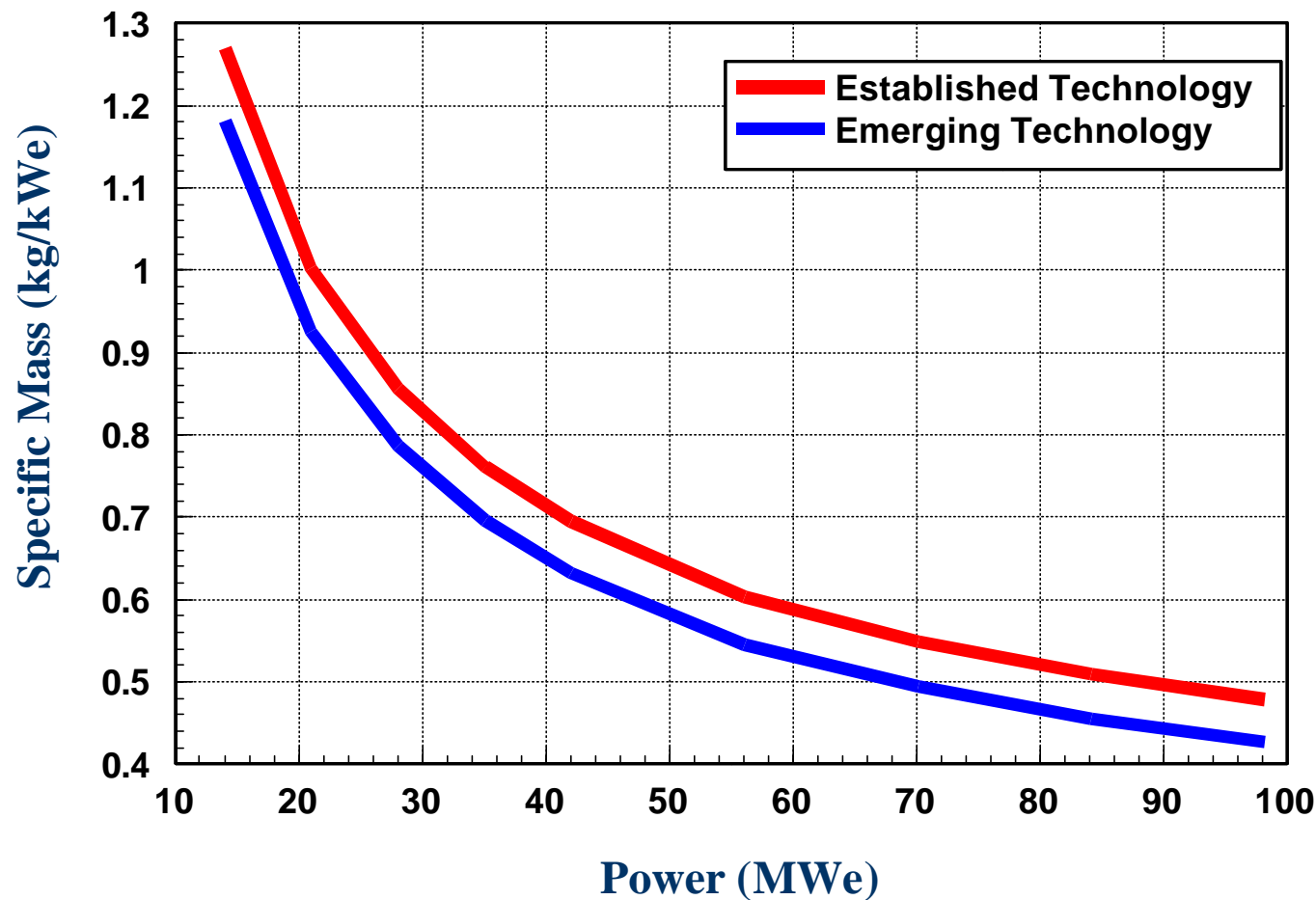
MCNP Reactor & Shield Model



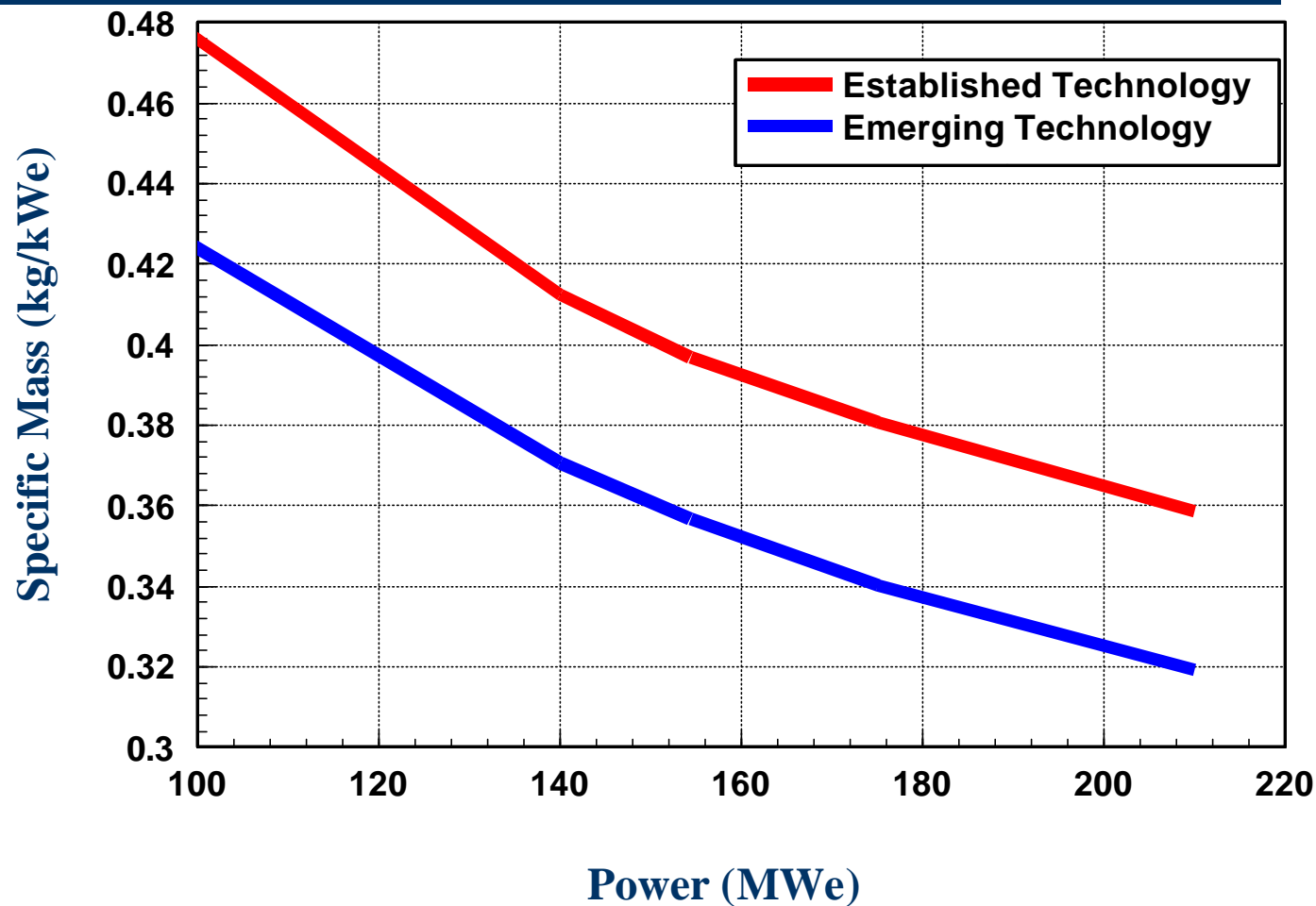
Fissioning Plasma Core Reactor Weight Performance (<1kg/kWe for >20MWe)



Fissioning Plasma Core Reactor Weight Performance ($<1\text{kg/kWe}$ for $>20\text{MWe}$)



Fissioning Plasma Core Reactor Weight Performance (<0.5 kg/kWe for >100 MWe)



Specific Mass Estimates Utilizing Advanced/Emerging Technologies

| Power (MWe) | 21 | 40 | 60 | 80 | 100 | 200 |
|--------------------------|-----------|-----------|-----------|-----------|------------|------------|
| Reactor (MT) | 7.77 | 10.23 | 12.26 | 14.11 | 15.75 | 22.42 |
| Shield (MT) | 5.30 | 6.52 | 7.65 | 8.78 | 9.86 | 14.98 |
| Radiators (MT) | 0.54 | 1.01 | 1.50 | 2.02 | 2.53 | 5.05 |
| Structural (MT) | 1.46 | 1.99 | 2.45 | 2.87 | 3.25 | 4.81 |
| Pumps (MT) | 0.66 | 1.23 | 1.84 | 2.46 | 3.09 | 6.16 |
| MHD Gen. (MT) | 3.00 | 3.72 | 4.24 | 4.68 | 5.05 | 6.36 |
| Total (MT) | 18.73 | 24.69 | 29.94 | 34.92 | 39.52 | 59.78 |
| Sp. Mass (kg/kWe) | 0.89 | 0.62 | 0.50 | 0.44 | 0.39 | 0.30 |

Fissioning Plasma Core Reactor Weight Performance

| Core Volume 3.0 m ³ | | | | | | |
|--------------------------------|--------------------------------------|---------------------|------------------------|--------------------------------------|---------------------|------------------------|
| Power/Core Pressure | 210 MWe / P _{core} =40 atm. | | | 151 MWe / P _{core} =30 atm. | | |
| | Current Established | Current Advanced | Emerging Technology | Current Established | Current Advanced | Emerging Technology |
| Reactor (MT) | 22.9 | 22.9 | 22.9 | 22.9 | 22.9 | 22.9 |
| Shield (MT) | 15.4 | 15.4 | 15.4 | 15.4 | 15.4 | 15.4 |
| Radiators (MT) | 23.4 | 15.7 | 15.7 | 17.6 | 11.8 | 11.8 |
| Vessel/Struct. (MT) | 7.1 | 4.9 | 4.5 | 7.1 | 4.9 | 4.5 |
| Pumps (MT) | 1.72 | 1.72 | 1.72 | 1.36 | 1.36 | 1.36 |
| MHD Gen. (MT) | 6.46 | 6.46 | 6.46 | 5.79 | 5.79 | 5.79 |
| Total mass (MT) | 77.1 | 67.2 | 66.8 | 70.2 | 62.2 | 61.8 |
| Specific Mass (kg/kWe) | 0.367 | 0.32 | 0.318 | 0.465 | 0.412 | 0.410 |

Fissioning Plasma Core Reactor Weight Performance

| Core Volume 2.5 m ³ | | | | | | |
|--------------------------------|--------------------------------------|---------------------|------------------------|--------------------------------------|---------------------|------------------------|
| Power/Core Pressure | 175 MWe / P _{core} =40 atm. | | | 126 MWe / P _{core} =30 atm. | | |
| | Current Established | Current Advanced | Emerging Technology | Current Established | Current Advanced | Emerging Technology |
| Reactor (MT) | 20.9 | 20.9 | 20.9 | 20.9 | 20.9 | 20.9 |
| Shield (MT) | 13.7 | 13.7 | 13.7 | 13.7 | 13.7 | 13.7 |
| Radiators (MT) | 19.5 | 13.1 | 13.1 | 14.6 | 9.8 | 9.8 |
| Vessel/Struct. (MT) | 6.4 | 4.5 | 4.1 | 6.4 | 4.5 | 4.1 |
| Pumps (MT) | 1.48 | 1.48 | 1.48 | 1.18 | 1.18 | 1.18 |
| MHD Gen. (MT) | 6.08 | 6.08 | 6.08 | 5.45 | 5.45 | 5.45 |
| Total mass (MT) | 68.1 | 59.7 | 59.3 | 62.3 | 55.5 | 55.2 |
| Specific Mass (kg/kWe) | 0.389 | 0.341 | 0.339 | 0.495 | 0.441 | 0.438 |

Fissioning Plasma Core Reactor Weight Performance

| Core Volume 2.0 m ³ | | | | | | |
|--------------------------------|--------------------------------------|---------------------|------------------------|--------------------------------------|---------------------|------------------------|
| Power/Core Pressure | 140 MWe / P _{core} =40 atm. | | | 101 MWe / P _{core} =30 atm. | | |
| | Current Established | Current Advanced | Emerging Technology | Current Established | Current Advanced | Emerging Technology |
| Reactor (MT) | 18.8 | 18.8 | 18.8 | 18.8 | 18.8 | 18.8 |
| Shield (MT) | 12.0 | 12.0 | 12.0 | 12.0 | 12.0 | 12.0 |
| Radiators (MT) | 15.6 | 10.4 | 10.4 | 11.8 | 7.9 | 7.9 |
| Vessel/Struct. (MT) | 5.8 | 3.9 | 3.6 | 5.8 | 3.9 | 3.6 |
| Pumps (MT) | 1.24 | 1.24 | 1.24 | 1.01 | 1.01 | 1.01 |
| MHD Gen. (MT) | 5.64 | 5.64 | 5.64 | 5.06 | 5.06 | 5.06 |
| Total mass (MT) | 59.0 | 52.0 | 51.7 | 54.4 | 48.7 | 48.4 |
| Specific Mass (kg/kWe) | 0.421 | 0.372 | 0.370 | 0.538 | 0.482 | 0.479 |

Summary

- VCR-MHD gives *direct* energy conversion at highest quality.
- MHD takes advantage of non-equilibrium ionization.
- Vapor Core @ High or Ultrahigh Temperature, meaning...
- Less costly radiators for heat rejection.
- Combined VCR-MHD space power might have very low specific mass, $M_{sp} \approx 0.5 \text{ kg/kW}_e$.
- A magnetoplasmadynamic rocket can achieve high specific impulse, $I_{sp} \approx 10,000 \text{ s}$.
- VASIMR propelled craft would need 100's of Megawatts — a VCR-MHD power supply can deliver.
- VASIMR has variable I_{sp} allowing for flexible abort scenarios.

Summary in Brief

- Direct energy conversion — Highest Quality.
- Low specific mass, M_{sp} .
- High specific impulse, I_{sp} .
- VCR-MHD power matching with VASIMR.
- Most materials are available.